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ABSTRACT

This work presents a stable locomotion of a 12 DoF biped using motion planning of its Centre of Mass (CoM). The biped is modelled as a 3-D Linear Inverted Pendulum (LIP). The walking pattern is generated using the CoM motion planner and foot pattern generator so that the CoM stays inside the Support Polygon (SP) created by feet during the locomotion. Ultimately, simulation and hardware results of biped locomotion using the proposed methodology are presented.

1 INTRODUCTION

Biped locomotion has inherent challenges because of its hybrid dynamics, effective underactuation and joint space control [1]. There exists more than one stability criterion which researchers have followed to achieve stable locomotion over the year, such as Zero Moment Point (ZMP) [2], limit cycle [3], Capture Point(CP) [4] etc. All criteria have limitations, e.g., ZMP [5] based criterion cannot be used straightforwardly for non-level surfaces, and limit cycle criterion is best suited for periodic locomotions. etc. However, a CoM-based criterion can be applied universally if the walking speed is sufficiently low. In the present work, stable locomotion of a biped is generated based on its CoM motion and foot pattern generator. Here, we have presented locomotion on level ground only, but the same criteria can be applied to walking on any surfaces because of using the CoM planner. This criterion was used earlier for quasi-static motion. However, it can also be used for locomotion with high speed if we can choose allowable CoM locations more conservatively.

2 METHODOLOGY

In the present work, we have generated CoM and, subsequently, the hip joint motion of a biped using the LIP model. The equations of CoM motion are

$$x_c(t) = x_c(0)\cosh(\frac{t}{T_c}) + T_c \dot{x}_h(0)\sinh(\frac{t}{T_c}), \quad y_c(t) = y_c(0)\cosh(\frac{t}{T_c}) + T_c \dot{y}_h(0)\sinh(\frac{t}{T_c})$$
(1)

where $x_c(t)$ and $y_c(t)$ denote x and y- coordinate of the biped's CoM at time t, and $T_c = \frac{z_c}{g}$ (z_c is zcoordinate of CoM). From the CoM trajectory, torso CoM motions and, subsequently, hip joint motions are obtained with an assumption that the distance between the torso's CoM and the biped's CoM remains the same throughout the locomotion. The foot-pattern generator equation for n-th step is written as

$$x_f^n = s_x^{(n+1)}/2, \quad y_f^n = (-1)^n s_y^{(n+1)}/2, \quad z_f^n = 0,$$
 (2)

Using equation (2), the ankle motion of the support leg is obtained. The swing leg's ankle motion is obtained as

$$x_a = -s_l \cos(\frac{\pi}{T}t), \quad z_a = \frac{h_f}{2} [1 - \cos(\frac{\pi}{t}t)]$$
 (3)

where x_a and z_a are x and z coordinates of the ankle joint respectively. The variables s_l , h_f , and T denote step length, swing leg clearance and step time, respectively. After obtaining ankle and hip motion, inverse kinematics is performed to obtain the required joint trajectories. The joint trajectories are input to the system using position control. The generated biped locomotion using this methodology is shown next.



Figure 1. Snaps from Biped locomotion: (a) Simulation in Pybullet, (b) Hardware.

3 RESULTS

Figure 1 shows snaps from the locomotion in simulation and hardware, respectively. The simulation is performed in Pybullet. For the hardware, Pybullet communicates the joint trajectories to an Arduino Microcontroller in real time. Then, Arduino sends the PWM signal to servo motors. The videos for the same is available here.

4 CONCLUSIONS

Using the proposed methodology, stable quasi-static locomotion of a biped on a level ground is shown in this work. This work will be extended to locomotions with larger step lengths, higher walking speeds, and various surfaces.

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